

## SOLUTIONS

### MIDTERM EXAM I

Nov 21, 2015

110 min

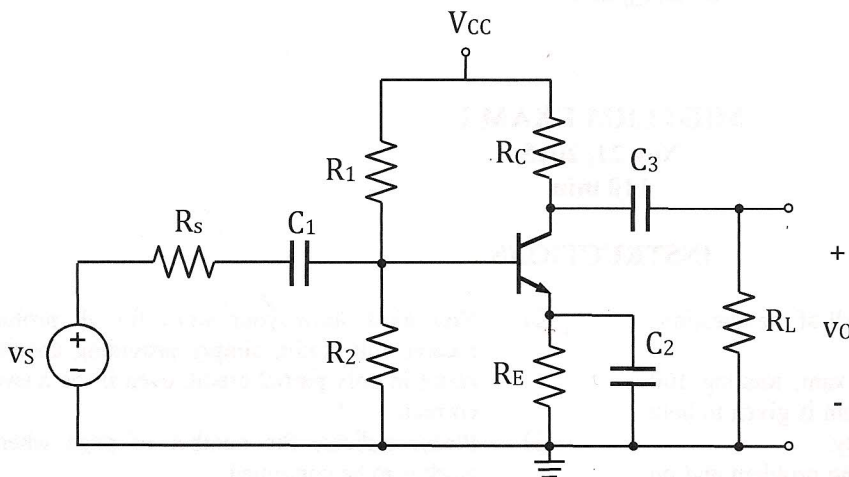
#### INSTRUCTIONS

- |  |   |
|--|---|
| <ul style="list-style-type: none"> <li> Read all of the instructions and all of the questions before beginning the exam.</li> <li> There are 5 questions on this exam, totaling 100 points. The credit for each problem is given to help you allocate your time accordingly.</li> <li> Do not spend all your time on one problem and on one part and attempt to solve all of them.</li> <li> Calculators are allowed, but borrowing is not allowed.</li> <li> Your mobile phones must be turned off during the exam.</li> <li> Turn in the entire exam, including this cover sheet.</li> </ul> | <ul style="list-style-type: none"> <li> You must show your work for all problems to receive full credit; simply providing answers will result in only partial credit, even if the answers are correct.</li> <li> Please indicate the number of page where your work is to be continued.</li> <li> Put your name on any additional material that you submit.</li> <li> Be sure to provide units where necessary.</li> <li> Please sign the honor pledge that is provided below.</li> </ul> |
|--|---|

	Question	Points	Grade
Last Name : .....	1	25	
Name : .....	2	25	
Section : .....	3	30	
Student No : .....	4	20	
	TOTAL	100	

The basic equations of the output characteristics of an NMOS transistor		
$V_{GS}$	$V_{DS}$	$I_D$
i) $V_{GS} < V_{Tn}$	-	0
ii) $V_{GS} > V_{Tn}$	a) $V_{DS} < V_{GS} - V_{Tn}$	$K_n [ 2(V_{GS} - V_{Tn})V_{DS} - V_{DS}^2 ]$
	b) $V_{GS} - V_{Tn} \leq V_{DS}$	$K_n (V_{GS} - V_{Tn})^2$
where $K_n = \frac{K'_n}{2} \left( \frac{W}{L} \right)$ and $K'_n = \mu_n C_{ox}$		

Q1. Consider the common-emitter amplifier given below.



Circuit Parameters

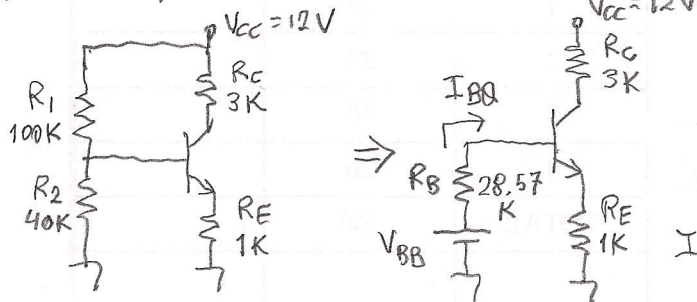
- $V_{CC} = 12\text{ V}$
- $R_S = 1\text{ k}\Omega$
- $R_1 = 100\text{ k}\Omega$
- $R_2 = 40\text{ k}\Omega$
- $R_C = 3\text{ k}\Omega$
- $R_E = 1\text{ k}\Omega$
- $R_L = 10\text{ k}\Omega$

Transistor Parameters

- $V_{BE(ON)} = 0.7\text{ V}$
- $\beta = 100$
- $V_A = 50\text{ V}$
- $V_{CE(SAT)} = 0$
- $V_T = 26\text{ mV}$

- (a) Determine the Q point values  $V_{CEQ}$  and  $I_{CQ}$ .
- (b) Determine the AC small signal voltage gain  $A_v = v_o/v_s$ .
- (c) Draw the DC and AC load lines.
- (d) Determine maximum peak value of the undistorted swing at the output.

(a) DC Equivalent Circuit



$$R_B = 100\text{K} // 40\text{K} = \frac{(100)(40)}{140} = 28.57\text{K}$$

$$V_{BB} = \frac{40}{140} \cdot 12\text{V} = 3.43\text{ V}$$

$$I_{BQ} = \frac{V_{BB} - V_{BE}}{R_B + (\beta + 1)R_E} = \frac{3.43 - 0.7}{28.57 + 101} = \frac{2.73\text{ V}}{129.5\text{ K}}$$

$$I_{BQ} = 21.08\text{ }\mu\text{A}$$

$$I_{CQ} = \beta I_{BQ} = 2.1\text{ mA} \Rightarrow V_{CEQ} = V_{CC} - R_C I_{CQ} - R_E I_{EQ} = 12 - (3)(2.1) - (1)(2.12)$$

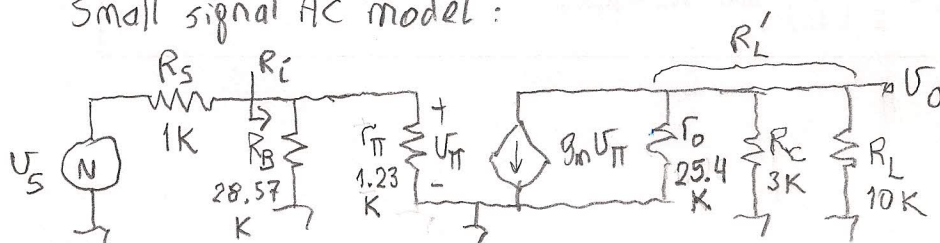
$$V_{CEQ} = 3.58\text{ V} \quad (V_{CEQ} > V_{CE(SAT)}) \text{ ; Forward active!}$$

(b) Small signal parameters :

$$r_{\pi} = \frac{V_T}{I_{BQ}} = \frac{26\text{ mV}}{21.08\text{ }\mu\text{A}} = 1.23\text{ K} \Rightarrow g_m = \frac{\beta}{r_{\pi}} = 81.3\text{ mS}$$

$$r_o = \frac{V_A + V_{CEQ}}{I_{CQ}} = \frac{53.58\text{ V}}{2.1\text{ mA}} = 25.4\text{ K}$$

Small signal AC model :



$$R_i = R_B // r_{\pi} = \frac{(28.57)(1.23)}{28.57 + 1.23} = 1.18 \text{ K}$$

$$R_L' = r_o // R_C // R_L = 2.12 \text{ K}$$

$$V_{\pi} = \frac{R_i}{R_S + R_i} V_S = \frac{1.18}{2.18} V_S = 0.54 V_S$$

$$V_o = -g_m V_{\pi} R_L' = (-81 \text{ mS})(2.12 \text{ K}) = -171.7 V_{\pi}$$

$$A_v = \frac{V_o}{V_S} = -92.9$$

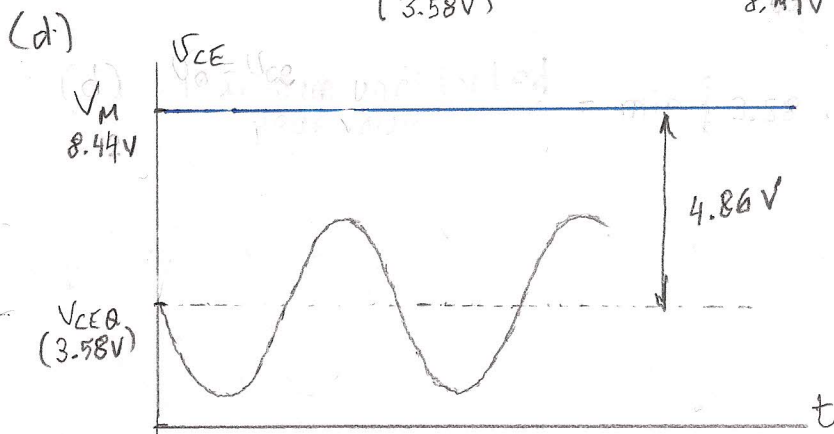
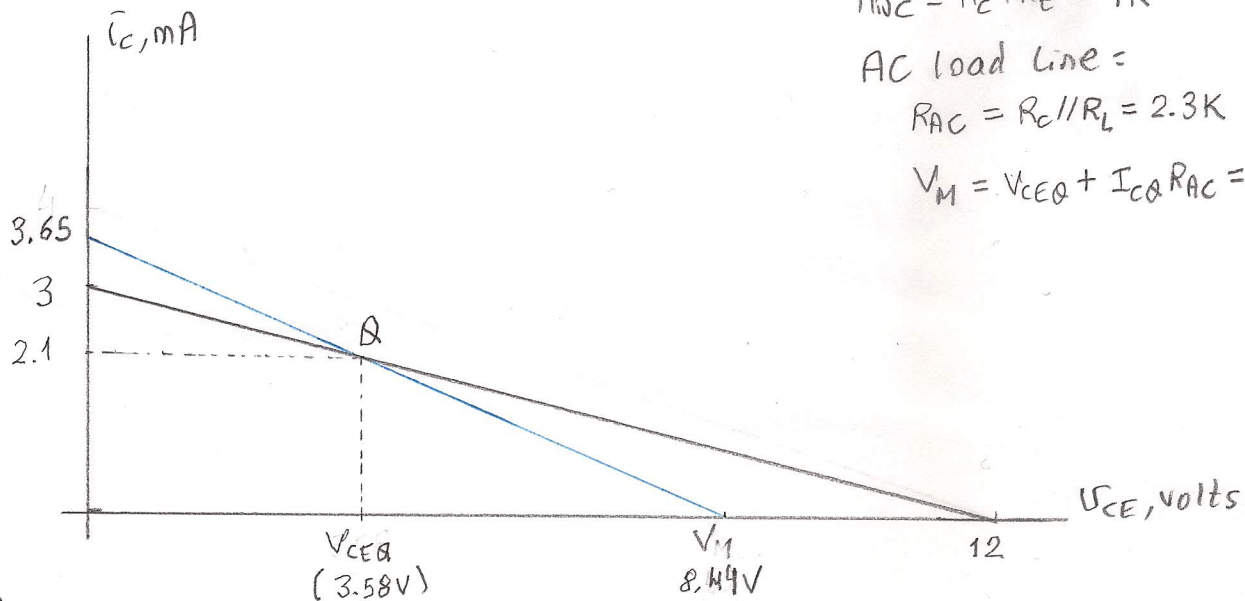
(c) DC load line equation:  $V_{CC} = I_C R_C + V_{CE} + R_E I_E \approx V_{CE} + (R_C + R_E) I_C$

$$R_{DC} = R_C + R_E = 4 \text{ K}$$

AC load line:

$$R_{AC} = R_C // R_L = 2.3 \text{ K}$$

$$V_M = V_{CEQ} + I_{CQ} R_{AC} = 8.44 \text{ V}$$



Output signal is around  $V_{CEQ}$ .

Positive peaks will be limited by 8.42V (peak value =  $8.44 - 3.58 = 4.86 \text{ V}$ )

Negative peaks will be limited by 3.58V

Then the maximum undistorted swing on both sides will be limited to 3.58V.

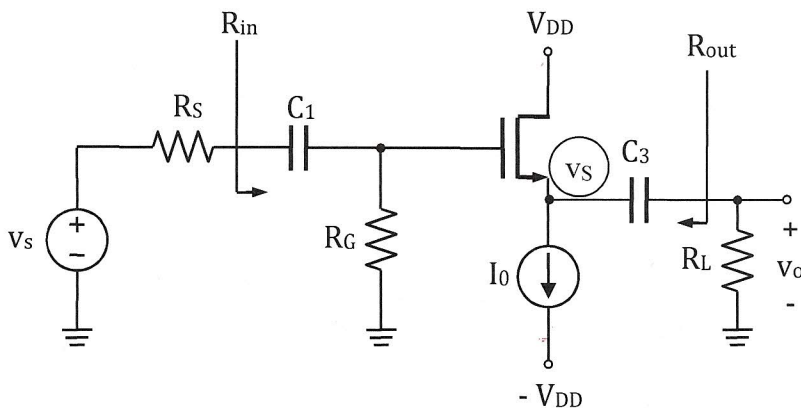
The output signal and the corresponding input signal

$$V_{CE} = V_{CEQ} + v_{ce} = V_{CEQ} + V_o = 3.58 - 3.58 \sin \omega t \text{ volts}$$

$$V_o = -3.58 \sin \omega t \text{ volts} = A_v V_S \Rightarrow V_S = -\frac{3.58}{-92.9} \sin \omega t \text{ volts} = 38.5 \sin \omega t \text{ mV}$$



**Q2. (25 pts)** Consider the common drain (source follower) circuit given below.



Circuit Parameters

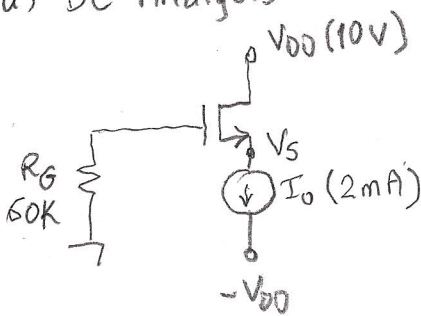
- $V_{DD} = 10 \text{ V}$
- $I_0 = 2 \text{ mA}$
- $R_S = 5 \text{ k}\Omega$
- $R_G = 60 \text{ k}\Omega$
- $R_L = 5 \text{ k}\Omega$

Transistor Parameters

- $V_{Tn} = 1 \text{ V}$
- $K_n = 8 \text{ mA/V}^2$
- $V_A = 100 \text{ V}$

- a) Determine the quiescent point values  $V_{DSQ}$  and  $I_{DQ}$ . (Check SAT condition!)
- b) Determine the small signal parameters  $g_m$  and  $r_o$ .
- c) Draw the AC small signal model of the circuit.
- d) Determine the small signal voltage gain  $A_v = v_o/v_s$ .
- e) Determine the input resistance  $R_{in}$  and the output resistance  $R_{out}$ .
- f) Determine the total source voltage  $v_s$ .

(a) DC Analysis



Assume SAT =  
 $I_{DS} = I_0 = K_n (V_{GSQ} - V_{TN})^2 \quad I_{DQ} = I_0 = 2 \text{ mA}$

$$2 = 8 (V_{GSQ} - 1)^2$$

$$\frac{1}{2} = V_{GSQ} - 1 \Rightarrow V_{GSQ} = 1.5 \text{ V}$$

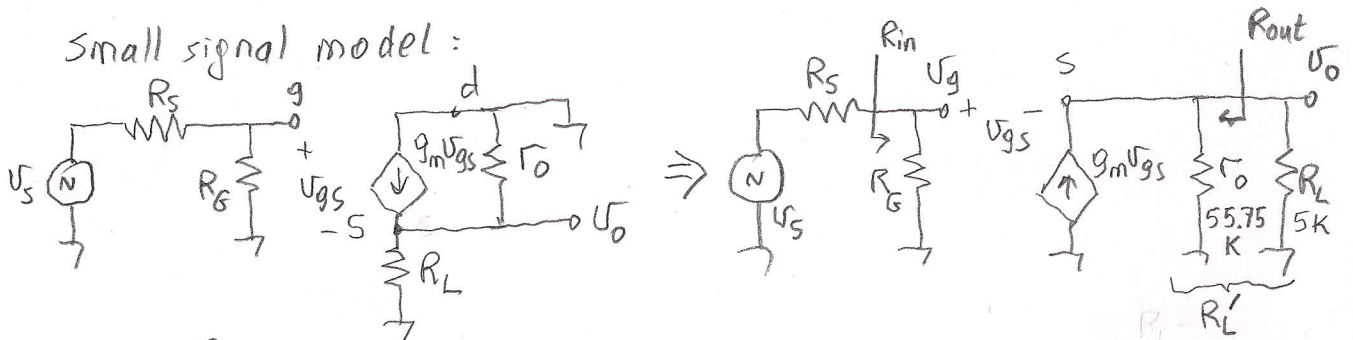
$$\left. \begin{aligned} V_{GSQ} &= -V_{GSQ} = -1.5 \text{ V} \\ V_{DQ} &= V_{DD} = 10 \text{ V} \end{aligned} \right\} \begin{aligned} V_{DSQ} &= V_{DD} - V_{GSQ} \\ &= 11.5 \text{ V} > V_{GSQ} - V_{TN} = 0.5 \text{ V} \end{aligned}$$

SAT assumption is satisfied.

(b)  $g_m = 2K_n (V_{GSQ} - V_{TN}) = (2)(8 \text{ mA/V}^2)(1.5 - 1) \text{ V} = 8 \text{ mA/V}$

$$r_o = \frac{V_A + V_{DSQ}}{I_{DQ}} = \frac{100 + 11.5}{2} = 55.75 \text{ K}$$

(c) Small signal model:



$$V_g = \frac{R_G}{R_s + R_G} v_s = \frac{60}{5 + 60} v_s = 0.92 v_s$$

$$R'_L = r_o // R_L = (55.75 \text{ K}) // (5 \text{ K}) = 4.59 \text{ K}$$

$$(d) \quad V_o = g_m V_{gs} R_L' = g_m R_L' (V_g - V_s)$$

$$V_o = V_s \Rightarrow V_o = g_m R_L' V_g - g_m R_L' V_o$$

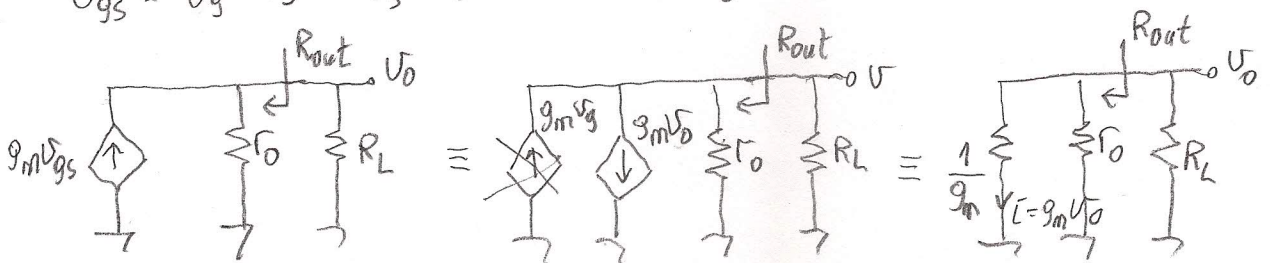
$$(1 + g_m R_L') V_o = g_m R_L' V_g$$

$$A_v = \frac{V_o}{V_g} = \frac{g_m R_L'}{1 + g_m R_L'} = \frac{(8)(4.59)}{1 + (8)(4.59)} = 0.97$$

$$(e) \quad R_{in} = R_G = 60K$$

To determine  $R_o$ , let  $V_s = 0$ . Then  $V_g = 0$

$$V_{gs} = V_g - V_s = V_g - V_o \text{ since } V_o = V_s$$



$$R_{out} = \frac{1}{g_m} \parallel r_o = \left( \frac{1}{8 \text{ mA/V}} \right) \parallel 55.75K = 0.125K \parallel 55.75K \approx 0.125K$$

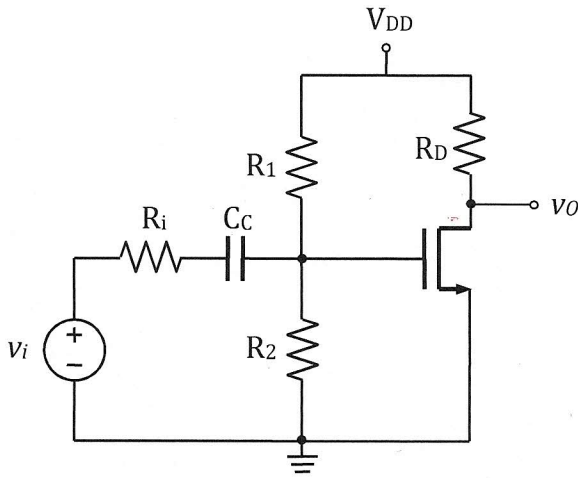
since  $55.75K \gg 0.125K$

$$(f) \quad V_{SQ} = -V_{GSQ} = -1.5V$$

$$V_g = V_{SQ} + V_s = V_{SQ} + V_o = -1.5V + A_v V_s = -1.5V + 0.97 V_s$$

**Q3. (30 pts)** For the MOSFET circuit given below,

- i. Determine the small signal parameters and draw the low frequency small signal model.
- ii. Determine the lower corner frequency.
- iii. Find the midband voltage gain.
- iv. Plot the low frequency magnitude response.



The transistor Parameters

$$V_{TN} = 0.5 \text{ V}$$

$$K_N = 2 \text{ mA/V}^2$$

$$\lambda = 0$$

Circuit Parameters

$$V_{DD} = 10 \text{ V}$$

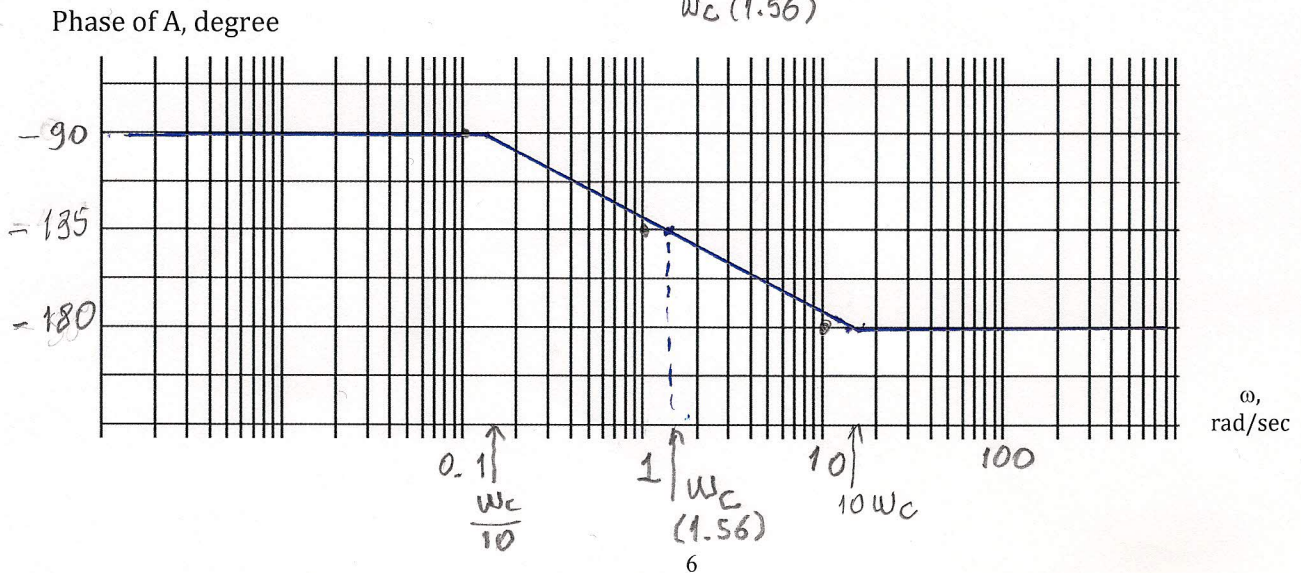
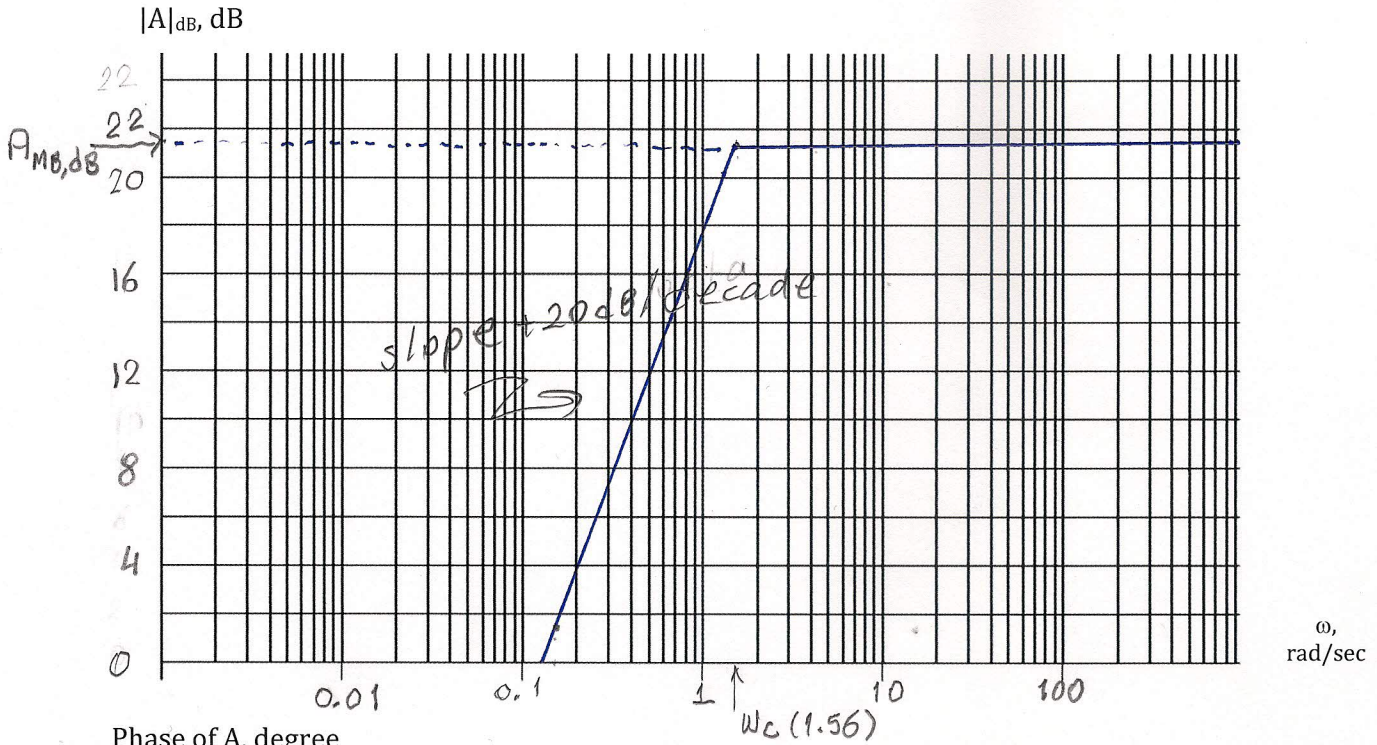
$$R_i = 1 \text{ k}\Omega$$

$$R_1 = 850 \text{ k}\Omega$$

$$R_2 = 150 \text{ k}\Omega$$

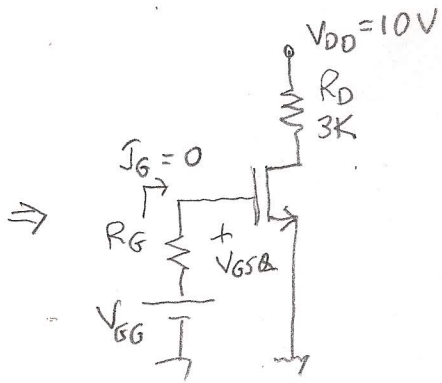
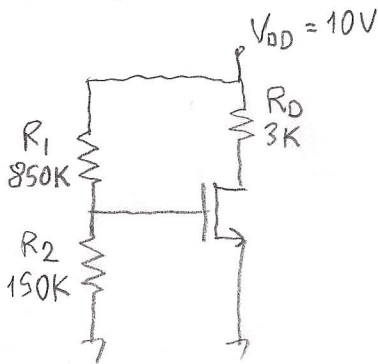
$$R_D = 3 \text{ k}\Omega$$

$$C_c = 5 \text{ }\mu\text{F}$$





(i) DC Analysis



$$V_{GG} = \frac{R_2}{R_1 + R_2} V_{DD} = \frac{150}{1000} \cdot 10V = 1.5V$$

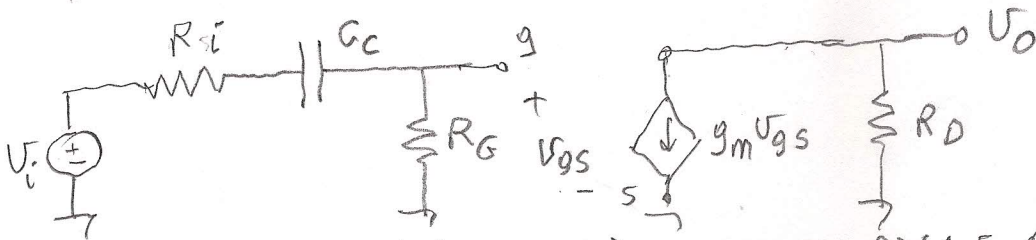
$$R_G = 850K // 150K = 127.5K$$

$$V_{GSB} = V_{GG} = 1.5V \quad (\text{since } I_G = 0)$$

$$I_{DSB} = K_N (V_{GSB} - V_{TN})^2 = (2 \text{ mA/V}^2) (1.5 - 0.5)^2 = 2 \text{ mA}$$

$$V_{DSB} = V_{DD} - I_{DSB} R_D = 10 - (3K)(2 \text{ mA}) = 4V > V_{GSB} - V_{TN} = 1V \quad (\text{SAT V})$$

b. Low frequency small signal model:



$$g_m = 2K_N (V_{GSB} - V_{TN}) = (2)(2 \text{ mA/V}^2)(1.5 - 0.5V) = 4 \text{ mA/V}$$

$$r_o = \frac{1}{\lambda I_{DSB}} = \infty$$

$$(ii) \quad \omega_c = \frac{1}{C_c R_{eq}} \quad ; \quad R_{eq} = R_i + R_G = 1 + 127.5 = 128.5 \text{ K}$$

$$\omega_c = \frac{1}{(5 \times 10^{-6})(128.5 \times 10^3)} = 1.56 \text{ rad/sec}$$

$$(iii) \quad V_{gs} = \frac{R_G}{R_i + R_G} V_i \quad ; \quad V_o = -g_m V_{gs} R_D = -g_m R_D \frac{R_G}{R_i + R_G} V_i$$

$$A_{MB} = -(4)(3) \frac{128.5}{129.5} = -11.9 \Rightarrow \text{Phase}$$

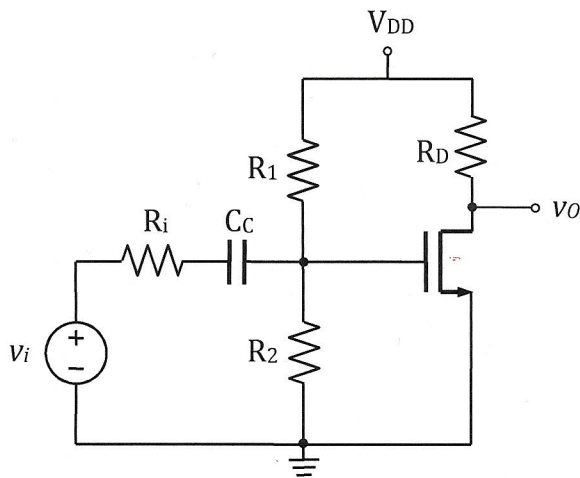
$$A_{MB, dB} = \frac{A_{MB}}{1 + j(\omega/\omega_c)} \quad (A_{MB, dB} = 20 \log(11.9) = 21.5 \text{ dB})$$

$$\theta = -180^\circ + 90^\circ - \tan^{-1} \left( \frac{\omega}{\omega_c} \right) = -90^\circ - \tan^{-1} \left( \frac{\omega}{\omega_c} \right)$$

Magnitude  
 (-) sign (j term) denominator  
 Plots are on the previous page.

**Q4. (20 pts)** Consider the MOSFET circuit given in Question 3 above.

- i. Draw the simplified high-frequency equivalent circuit.
- ii. Determine the higher corner frequency.
- iii. Plot the overall frequency response.



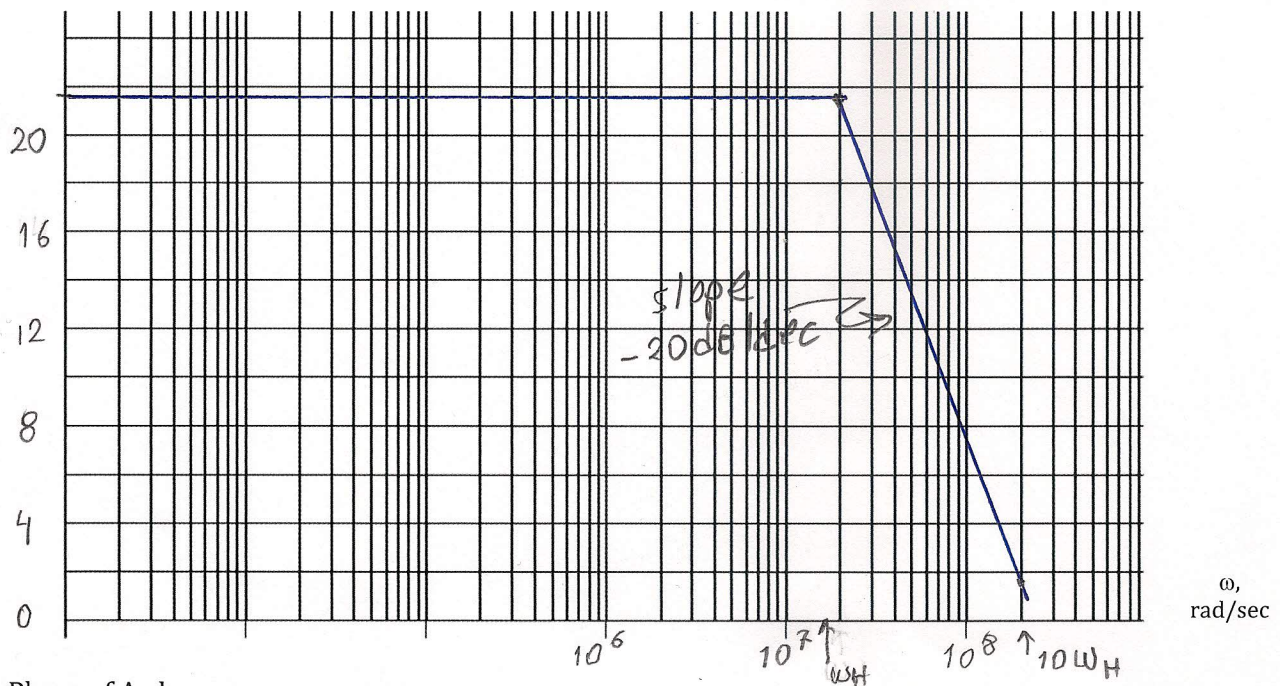
The transistor Parameters  
(As given in Q3.)

Circuit Parameters  
(As given in Q3)

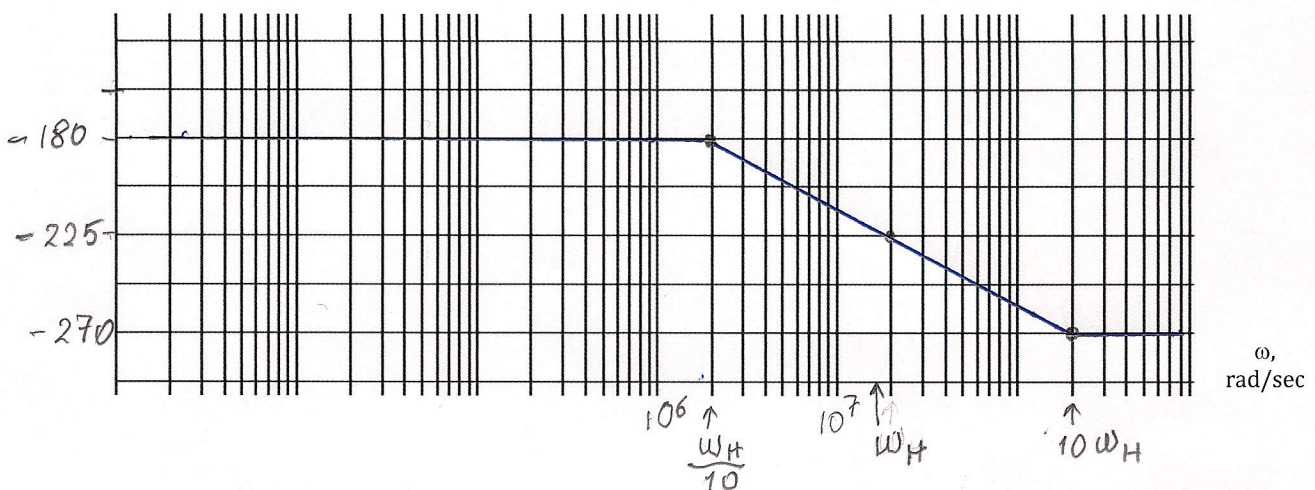
$$C_{gs} = 10 \text{ pF}$$

$$C_{gd} = 4 \text{ pF}$$

$|A|_{dB}, \text{ dB}$



Phase of A, degree





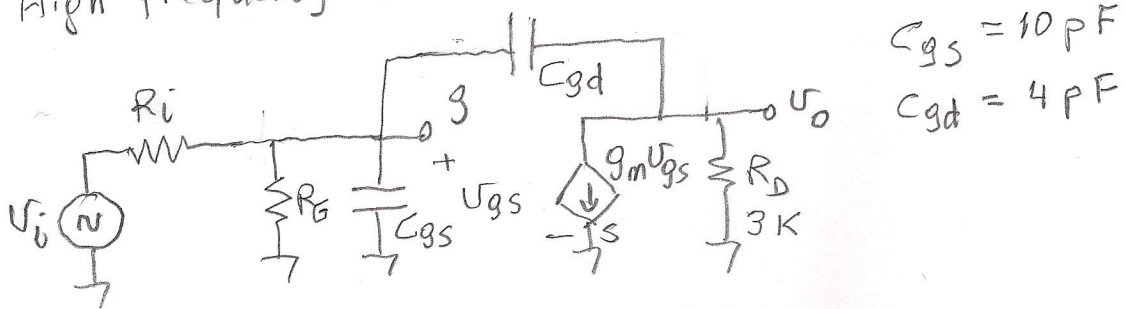
i) DC Analysis : (From Q3)

$$V_{GSQ} \approx 1.5V, I_{DQ} = 2mA, V_{DSQ} = 4V \text{ (SAT V)}$$

AC Analysis

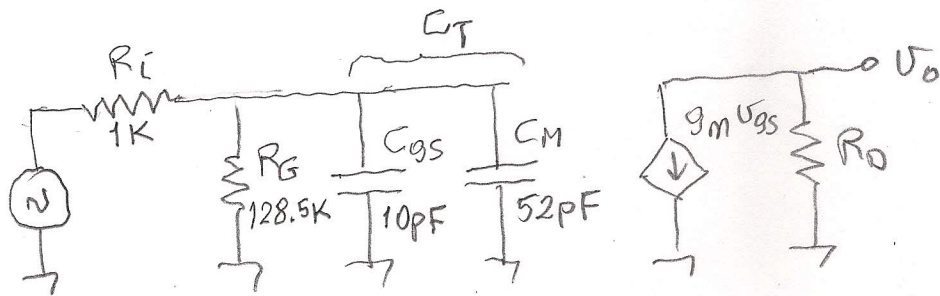
$$g_m = 4mA/V$$

High frequency model : ( $C_c$  is short)



$$C_{gs} = 10pF$$

$$C_{gd} = 4pF$$



$$C_M = C_{gd} (1 + g_m R_D) = (4pF) (1 + 4 \cdot 3) = 52pF$$

$$C_T = C_{gs} + C_M = 62pF$$

ii)  $\omega_H = \frac{1}{C_T R_{eq}}$   $R_{eq} = R_G // R_i \approx 1K$  (Corner frequency)

$$\omega_H = \frac{1}{(52 \times 10^{-12})(10^3)} = \frac{10^9}{62} = 16.26 \text{ Mrad/sec}$$

iii.  $A_v = \frac{A_{MB}}{1 + j(\frac{\omega}{\omega_H})} = \frac{-11.9}{1 + j(\frac{\omega}{\omega_H})}$

$$A_{MB} = 11.9 \Rightarrow A_{MB, dB} = 22.5 \text{ dB Midband}$$

$$\theta = -180^\circ - \tan^{-1}\left(\frac{\omega}{\omega_H}\right) \text{ (Phase)}$$

Plots (-) sign denominator plots are on the left.